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(71) Applicant: **SHELL INTERNATIONALE RESEARCH  
MAATSCHAPPIJ B.V. [NL/NL]; Carel van Bylandtlaan  
30, NL-2596 HR The Hague (NL).**

(72) Inventors: **DE KEYZER, Noel, Raymond, Maurice;  
Avenue Jean-Monnet 1, Louvain-La-Neuve, B-1348 Ottig-  
nics (BE). STONER, Carolyn, Ann; 16506 Monte Carlo  
Lane, Houston, TX 77053 (US).**

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**WO 01/00257 A1**

(54) Title: **HOT MELT PRESSURE SENSITIVE POSITIONING ADHESIVE (III)**

(57) Abstract: The present invention is a hot melt pressure sensitive positioning adhesive for use with an absorbent article. The adhesive contains from 5 to less than 15 percent by weight of a blend of a selectively hydrogenated block copolymer of styrene-(butadiene and or isoprene)-styrene and a homogeneous linear interpolymers of ethylene and at least one C<sub>3</sub>-C<sub>20</sub> alpha olefin having a density from 0.85 to 0.91 grams per cubic centimeter, a tackifying resin and a plasticizer.

HOT MELT PRESSURE SENSITIVE  
POSITIONING ADHESIVE (III)

Field of the Invention

This invention relates to hot melt pressure sensitive positioning adhesives for use with absorbent articles which are based on hydrogenated block copolymers of styrene and butadiene and/or isoprene. More particularly, the invention relates to such adhesives which incorporate interpolymers of ethylene and at least one C<sub>3</sub>-C<sub>20</sub> alpha olefin for improved viscosity and viscosity/temperature profile.

Background of the Invention

Positioning adhesives are used on disposable articles (absorbent articles) such as sanitary napkins, incontinent pads, bed pads, feminine pads, panty shields, and diaper inserts, where an adhesive layer is used to attach the article to a woven fabric substrate such as a supporting undergarment or bed sheet. The positioning adhesive is commonly applied to a release liner and transfer coated to the garment facing surface of the disposable article. The positioning adhesive must be capable of attaching to the undergarment to hold the article in place without transferring to or otherwise being deposited on the undergarment. Furthermore, the adhesive must not discolor, damage, or disturb the fibers of the garment.

The positioning adhesive must be a pressure sensitive adhesive that has a viscosity that permits it to readily flow onto and partially penetrate the particular surface to which it is applied. It must have good bond strength and high tack for initial placement of the article on the

undergarment but also must have the ability to avoid loss of adhesion over time due to temperature conditions.

Finally, these articles are sometimes used for long periods of times at body temperature and they can have the drawback that the hot melt adhesive gradually softens and penetrates into the undergarment to which the article is adhering. In this case, the adhesive force greatly increases and the cohesive force is reduced. This causes the adhesive layer to suffer cohesion breakdown when the article is removed and some adhesive remains on the undergarment. Prevention of this deposit of adhesive on the undergarment is accordingly a necessary prerequisite for a successful positionable hot melt adhesive composition.

Block copolymers of styrene and dienes such as butadiene or isoprene have been used for a number of years in positionable hot melt adhesive formulations. More recently, the material of choice for such adhesives in feminine care applications has been selectively hydrogenated block copolymers of styrene and butadiene such as KRATON G-1650 polymer (KRATON is a trademark), which is a commercially available selectively hydrogenated styrene-butadiene-styrene block copolymer.

With the term "selective hydrogenation" is meant that primarily the butadiene block is hydrogenated. Butadiene that has been polymerized by 1,4-addition yields "ethylene" units upon hydrogenation and butadiene that has been polymerized by 1,2-addition yields "butylene" units. Therefore, selectively hydrogenated styrene-butadiene-styrene block copolymers are commonly referred to as styrene-ethylene/butylene-styrene (SEBS) block copolymers.

Formulations based on these SEBS block copolymers have been found to have excellent adhesion to fabrics like cotton and nylon and have the advantage that they

leave no residue after peeling. The application viscosity of formulations using these polymers is acceptable but it would be advantageous to have a positionable adhesive formulation which has a lower melt viscosity in order to be able to lower the application temperature. This reduces the risk of degradation, char forming, and filter plugging. This also results in energy and cost savings, decreases maintenance costs, and reduces the amount of odor due to any volatiles coming from the adhesive formulation. The present invention provides such an improved positionable hot melt adhesive formulation.

#### Summary of the Invention

The present invention is a hot melt pressure sensitive positioning adhesive for use with an absorbent article. The adhesive comprises:

- (a) from 5 to less than 15 percent by weight, basis the total of (a), (b) and (c), of a blend of
  - (i) a selectively hydrogenated styrene-(butadiene and/or isoprene)-styrene block copolymer having either (I) a polystyrene block number average molecular weight of 20,000 or less, or (II) having a polystyrene block number average molecular weight greater than 20,000 and
  - (ii) a homogeneous linear or substantially linear interpolpolymer of ethylene and at least one C<sub>3</sub>-C<sub>20</sub> alpha olefin having a density from 0.85 to 0.91 grams per cubic centimeter; and
- (b) from 50 to 80 percent by weight, basis the total of (a), (b) and (c), of a tackifying resin which has an aromaticity such that the MMAP cloud point is either (I) at least 45 °C or (II) at least 70 °C; and
- (c) from 5 to 35 percent by weight, basis the total of (a), (b) and (c), of a plasticizer.

The weight ratio of the block copolymer and the interpolpolymer in (a) preferably ranges from 90:10 to

10:90, more preferably from 80:20 to 20:80, even more preferably from 60:40 to 40:60. In case the polystyrene block weight average molecular weight is in the range from 5500 to 9500 and the total weight average molecular weight is in the range from 65,000 to 95,000, the weight ratio preferably ranges from 60:40 to 90:10, more preferably from 80:20 to 90:10. The block copolymer of (i) may also be one in which the polystyrene block molecular weight is greater than 20,000. In such case, the tackifying resin must have an aromaticity wherein the MMAP cloud point is at least 70 °C.

In each embodiment, a second block copolymer or mixture of block copolymers can be added to the block copolymer of (i) to lower the viscosity. One option is to add a second polymer which has a diblock content of 20 to 70 percent by weight. A second option is to add a polymer which has a polystyrene content of less than 25 percent by weight, preferably 22 percent by weight or less, which lowers the viscosity irrespective of diblock content if the base hydrogenated styrene-butadiene and/or isoprene-styrene block copolymer has a polystyrene content of 25 percent by weight or more, preferably 30 percent by weight or more.

Another option is to add more than two block copolymers. For example, a blend of a styrenic triblock copolymer, plus a styrenic block copolymer containing diblock, and a styrenic block copolymer containing less than 25% polystyrene could be used. Additionally, styrenic diblock copolymers could be added or copolymers with an ethylene/propylene multiblock could be added. This list is not limitative and therefore, it can be appreciated that a wide variety of block copolymers are useful in this invention including ABA triblock structures, ABA/AB triblock/diblock structures,

AB diblock structures,  $(B)_n$  structures, ABAB tetrablock structures where the A endblock is a non-elastomeric polymer block, typically polystyrene, and B is ethylene/butylene (hydrogenated butadiene) or ethylene/propylene (hydrogenated isoprene). Also included in the list are polymers which are grafted with maleic anhydride.

#### Detailed Description of the Invention

One of the primary components of the positioning adhesive composition of the present invention is the above-described hydrogenated block copolymer which has two polystyrene endblocks and a saturated or hydrogenated polybutadiene and/or polyisoprene midblock. This selectively hydrogenated base block copolymer provides the primary load bearing capability of the adhesive composition. It is important that the polymer be hydrogenated so that the structural integrity of the polymer is preserved even if outside forces that cause degradation are encountered. The block copolymer may be hydrogenated as generally described in the prior art, preferably so as to reduce at least 90 percent of any olefinic double bonds in the polymer chains. Suitably at least 50 percent, preferably at least 70 percent, and more preferably at least 90 percent, most preferably at least 95 percent of the original olefinic unsaturation is hydrogenated.

Polymerization of butadiene and/or isoprene is typically carried out such that a polybutadiene and/or polyisoprene block is formed which is largely amorphous at use temperatures (usually body temperature) and does not contain excess crystallinity which would interfere with flexibility. For hydrogenated polybutadiene blocks it is generally best that the vinyl content before hydrogenation not be less than 18 percent by weight,

preferably not less than 30 percent by weight, because below that number, the crystallinity of the polymer is too high, giving a stiff polymer which is unsuitable for use in pressure sensitive adhesives.

5           The term "vinyl content before hydrogenation" refers to the fact that a conjugated diene is polymerized via 1,2-addition (in the case of butadiene - it would be 1,2-addition or 3,4-addition in the case of isoprene). Although a pure "vinyl" group is formed only in the case  
10 of 1,2-addition polymerization of 1,3-butadiene, the effects of 1,2-addition and 3,4-addition polymerization of isoprene (and similar addition for other conjugated dienes) on the final properties of the block copolymer will be similar. The term "vinyl" refers to the presence  
15 of a pendant vinyl group on the polymer chain before hydrogenation. The purpose here is to introduce chain branching and to reduce the size of the main polymer backbone (since some of the carbons in the diene are in the pendant group) which reduces the end to end length of  
20 the molecule and, in turn, its viscosity in the cement.

          Anionic polymerization of conjugated diene hydrocarbons with lithium initiators is well known as described in U.S. Patents Nos. 4,039,593 and Re. 27,145 which descriptions are incorporated herein by reference.  
25 Polymerization commences with a monolithium, dilithium, or polylithium initiator which builds a living polymer backbone at each lithium site. Typical living polymer structures containing polymerized conjugated diene hydrocarbons are:

30           X-B-Li  
            X-A-B-Li  
            X-A-B-A-Li  
            Li-B-Y-B-Li  
            Li-A-B-Y-B-A-Li

wherein B represents polymerized units of one or more conjugated diene hydrocarbons such as butadiene or isoprene, A represents polymerized units of one or more vinyl aromatic compounds such as styrene, X is the residue of a monolithium initiator such as sec-butyl-lithium, and Y is the residue of a dilithium initiator such as the diadduct of sec-butyllithium and m-diisopropenylbenzene. Some structures, including those pertaining to polylithium initiators or random units of styrene and a conjugated diene, generally have limited practical utility although known in the art.

The anionic polymerization of the conjugated diene hydrocarbons is typically controlled with structure modifiers such as diethylether or ethyl glyme (1,2-diethoxyethane) to obtain the desired amount of 1,2-addition (i.e. vinyl content). A 1,2-addition of about 40% may be achieved during polymerization at 50 °C with about 6% by volume of diethylether or about 200 ppm of ethyl glyme in the final solution. A 1,2-addition of about 47% may be achieved during polymerization by the presence of about 250 ppm of ortho-dimethoxybenzene (ODMB) in the final solution. A 1,2-addition of 78% may be achieved during polymerization by the presence of about 300 ppm of 1,2-diethoxypropane (DEP) in the final solution.

In general, the polymers useful in this invention may be prepared by contacting the monomer or monomers with an organoalkali metal compound in a suitable solvent typically, in the presence of a polar structure modifier in case an apolar solvent is used at a temperature in the range from -150 °C to 300 °C, preferably at a temperature in the range from 0 °C to 100 °C. Particularly effective polymerization initiators are organolithium compounds having the general formula:



RLi

wherein R is an aliphatic, cycloaliphatic, alkyl-substituted cycloaliphatic, aromatic or alkyl-substituted aromatic hydrocarbon radical having from 1 to 20 carbon atoms.

Suitable solvents include those useful in the solution polymerization of the polymer and include aliphatic, cycloaliphatic, alkyl-substituted cycloaliphatic, aromatic and alkyl-substituted aromatic hydrocarbons, ethers and mixtures thereof. Suitable solvents, then, include aliphatic hydrocarbons such as butane, pentane, hexane and heptane, cycloaliphatic hydrocarbons such as cyclohexane and cycloheptane, alkyl-substituted cycloaliphatic hydrocarbons such as methylcyclohexane and methylcycloheptane, aromatic hydrocarbons such as benzene and the alkyl-substituted aromatic hydrocarbons such as toluene and xylene and ethers such as tetrahydrofuran, diethylether and di-n-butyl ether.

When polar solvents like tetrahydrofuran are used, structure modifiers are typically not necessary for the preparation of high vinyl content butadiene and/or isoprene polymer blocks.

The hydrogenation of these polymers may be carried out by a variety of well established processes including hydrogenation in the presence of nickel catalysts such as Raney Nickel, noble metal catalysts such as those containing platinum and/or palladium and soluble transition metal catalysts. Suitable hydrogenation processes which can be used are ones wherein the diene-containing polymer or copolymer is dissolved in an inert hydrocarbon diluent such as cyclohexane and hydrogenated by reaction with hydrogen in the presence of a soluble hydrogenation catalyst. Such processes are disclosed in U.S. Patent Nos. 3,113,986, 4,226,952 and Reissue 27,145,

the disclosures of which are herein incorporated by reference. The polymers are most preferably hydrogenated in such a manner as to produce hydrogenated polymers having a residual unsaturation content in polydiene blocks of less than about 1 percent, and most preferably as close to 0 percent as possible, of their original unsaturation content prior to hydrogenation. A titanium catalyst such as disclosed in U.S. Patent No. 5,039,755, which is herein incorporated by reference, may also be used in the hydrogenation process.

The molecular weights of linear polymers or unassembled linear segments of polymers such as mono-, di-, triblock, etc., or the arms of star polymers before coupling are conveniently measured by Gel Permeation Chromatography (GPC), where the GPC system has been appropriately calibrated with polystyrene homopolymer standards (ASTM D 3536). For anionically polymerized linear polymers, the polymer is essentially monodisperse (weight average molecular weight/number average molecular weight ratio approaches unity), and it is both convenient and adequately descriptive to report the "peak" molecular weight of the narrow molecular weight distribution observed. Usually, the peak value is between the number and the weight average. The peak molecular weight is the molecular weight of the main species shown on the chromatograph. For polydisperse polymers the weight average molecular weight or number average molecular weight is calculated from the chromatograph and used. The materials used in the columns of the GPC are styrene-divinyl benzene gels or silica gels. The solvent is tetrahydrofuran and the detector is a refractive index detector.

As discussed above, the adhesive of the present invention contains from 5 to less than 15 percent by weight of a blend of a selectively hydrogenated block

copolymer of styrene and butadiene and/or isoprene and a homogeneous linear or substantially linear interpolpolymer of ethylene and a C<sub>3</sub>-C<sub>20</sub> alpha olefin. At least 5 percent is necessary to get the desired pressure sensitive adhesive properties and for the adhesive to be sufficiently cohesive. It is preferred that the maximum amount of the blend be less than 15 percent by weight in order to keep the viscosity of the adhesive sufficiently low for the positioning adhesive application. More polymer than 15 percent can be used and good adhesion properties will be obtained but the viscosity will be unnecessarily increased.

For block copolymers having a polystyrene block number average molecular weight of above 9500 and a total number average molecular weight of above 95,000 to 300,000, the block copolymer and interpolpolymer in the blend is preferably used in a weight ratio of 90:10 to 10:90. It is more preferred that the weight ratio range be from 20:80 to 80:20. A weight ratio range of 60:40 to 40:60 is most preferred because the best combination of properties is achieved in this range. For block copolymers having a polystyrene block number average molecular weight of 5500 to 9500 and a total number average molecular weight of 65,000 to 95,000, the weight ratio preferably ranges from 60:40 to 90:10, more preferably 80:20 to 90:10.

The base block copolymer must have a sufficient molecular weight and polystyrene content to be useful for pressure sensitive adhesives. Typically, the number average molecular weight is in the range from 65,000 to 300,000. If the molecular weight is less than 65,000 then the polymer loses its pressure sensitive adhesive properties. If the molecular weight is more than 300,000, then the polymer is less useful for adhesive

applications. The polystyrene content typically ranges from 11 to 40% by weight, more preferably 19 to 40% for the lower number average molecular weight (65,000 to 95,000) polymers because this confers the right balance of cohesion and processability to the polymer.

If the polystyrene block number average molecular weight is 20,000 or lower, then the tackifying resin which is used in the adhesive composition must have an aromaticity wherein the MMAP cloud point is at least 45 °C. If the polystyrene block molecular weight of the block copolymer is greater than 20,000, then the tackifying resin must have an aromaticity wherein the MMAP cloud point is at least 70 °C. If these aromaticity parameters are not satisfied, blends of the polymer, interpolymer and the tackifying resin are not phase stable, especially when aged for a few days at elevated temperature.

It is known that one method to characterize tackifying resin compatibility is by determination of cloud points in suitable solvent systems. From the cloud point values obtained, the resin may be characterized as being aliphatic, aromatic, or a combination of both, polar or nonpolar, and having a high or low molecular weight. Hydrocarbon resins display wide variation in cloud point values and thus the cloud point concept is a useful method to characterize hydrocarbon resins.

MMAP cloud point is a well-known measure of aromatic solubility and determines the aliphatic/aromatic character of the resin. The lower the MMAP cloud point value, which is expressed in degrees centigrade, the more aromatic is the resin. A 1:2 mixture of methylcyclohexane and aniline is used as the solvent system in the MMAP cloud point determination. A standard weight of resin is dissolved in the solvent at high temperature and allowed to cool with mixing. The temperature at which the resin

begins to separate out as an extra phase is determined to be the MMAP cloud point. This may be seen in the mixture as a cloudiness in the previously clear solution.

5 The viscosity of the adhesive formulation may be lowered by adding to the styrene-diene-styrene block copolymers described above from 5 to 40 percent by weight of a second block copolymer which has a diblock content of 20 to 70 percent by weight. Such block copolymers are often produced by making diblocks and then coupling them  
10 together. If the coupling efficiency is less than 100 percent, then the polymer will contain a certain amount of diblock. This is well known to those of ordinary skill in the art.

15 The viscosity of adhesive composition may also be lowered in the case where the styrene-diene-styrene block copolymer has a polystyrene content of more than 25 percent by weight, preferably 30 percent or more by weight, by adding to that block copolymer from 5 to 40 percent by weight of a second block copolymer which  
20 has a polystyrene content of less than 25 percent by weight, preferably 22 percent by weight or less. Also, the viscosity may be lowered by adding more than two styrenic block copolymers.

25 The second key component of the adhesive formulation of the present invention is the homogeneous linear or substantially linear interpolpolymer of ethylene and a C<sub>3</sub>-C<sub>20</sub> alpha olefin, having a density from 0.850 to 0.910 g/cm<sup>3</sup>. Generally, these interpolymers have a melt flow index of 0.1 to 100 dg/min (190 °C/2.16 kg),  
30 preferably 0.1 to 50 dg/min, more preferably 0.1 to 30 dg/min, most preferably 0.1 to 15 dg/min, and a polydispersity of less than 2.2. The interpolymers may have densities higher than the preferred range as long as

the resulting formulation has a viscosity and adhesive properties within the preferred range.

The term interpolymer is used herein to indicate a copolymer or a terpolymer. That is, at least one other comonomer is polymerized with ethylene to make the interpolymer. The homogeneous linear or substantially linear polymer is an ethylene polymer prepared using a constrained geometry or single site metallocene catalyst. By the term homogeneous, it is meant that any comonomer is randomly distributed within a given interpolymer molecule and substantially all of the interpolymer molecules have the same ethylene/comonomer ratio within that interpolymer. The melting peak of homogeneous linear and substantially linear ethylene polymers, as determined by differential scanning calorimetry (DSC), will broaden as the density decreases and/or as the number average molecular weight decreases. However, unlike heterogeneous polymers, when a homogeneous polymer has a melting peak greater than 115 °C (such as is the case of polymers having a density greater than 0.940 g/cm<sup>3</sup>) such polymers typically do not additionally have a distinct lower temperature melting peak. The homogeneous linear or substantial linear ethylene polymers are characterized as having a narrow molecular weight distribution ( $M_w/M_n$ ). For the linear and substantially linear ethylene polymers, the  $M_w/M_n$  is preferably from 1.5 to 2.5, preferably from 1.8 to 2.2.

Substantially linear ethylene polymers are homogeneous polymers having long chain branching. The long chain branches have the same comonomer distribution as the polymer backbone and can be as long as about the same length as the length of the polymer backbone. When a substantially linear ethylene polymer is employed in the practice of the invention, such polymer will be

characterized as having a polymer backbone substituted with from 0.1 to 3 long chain branches per 1000 carbons. Methods for determining the amount of long chain branching present, both qualitatively and quantitatively, are known in the art. For qualitative and quantitative methods for determination, see U.S. Patent Nos. 5,272,236 and 5,278,272 which are herein incorporated by reference.

The homogeneous linear or substantially linear ethylene polymer will be an interpolymer of ethylene with at least one alpha olefin. Preferred are interpolymers of ethylene with at least one C<sub>3</sub>-C<sub>20</sub> alpha olefin (for instance, propylene, isobutylene, 1-butene, 1-pentene, 1-hexene, 4-methyl-1-pentene, and 1-octene) with interpolymers of ethylene with at least one C<sub>4</sub>-C<sub>20</sub> alpha olefin, particularly at least one C<sub>6</sub>-C<sub>8</sub> alpha olefin, being most preferred. When 1-octene is employed as the comonomer, preferably the 1-octene is present in an amount greater than 14 percent by weight in the polymer as measured by NMR in accordance with ASTM D-5017. More preferably, the 1-octene comonomer content is greater than 20 percent by weight.

Homogeneously branched linear ethylene/alpha olefin interpolymers may be prepared by using polymerization processes which provide a homogeneous short chain branching distribution. For instance, see U.S. Patent No. 3,645,992 which is herein incorporated by reference. In this process, a soluble vanadium catalyst system is used. Others have used so-called single site metallocene catalyst systems to make such polymers. Substantially linear ethylene/alpha olefin interpolymers are available from the Dow Chemical Company and may be prepared in accordance with the techniques described in U.S. Patents Nos. 5,272,236 and 5,278,272 which are herein incorporated by reference.

Suitable tackifiers may be selected from the group consisting of compatible C<sub>5</sub> hydrocarbon resins, hydrogenated C<sub>5</sub> hydrocarbon resins, styrenated C<sub>5</sub> resins, styrenated C<sub>5</sub>/C<sub>9</sub> resins, styrenated terpene resins, fully hydrogenated or partially hydrogenated C<sub>9</sub> hydrocarbon resins, rosins esters, rosins derivatives and mixtures thereof. The tackifying resin must satisfy the MMAP requirements discussed above. Commercially available hydrocarbon tackifying resins for the present invention include PICCOTAC 95 (MMAP = 95 °C) as aliphatic resin, REGALREZ series, like REGALREZ 1085 (85 °C) or REGALREZ 6108 (54 °C) and REGALITE series, like REGALITE V-1100 (48 °C) or REGALITE S-260 (59 °C). REGALREZ 3102 resin (MMAP = 24 °C) does not work with any of these polymers because a phase stable blend cannot be achieved. (PICCOTAC, REGALREZ and REGALITE are trademarks.)

The suitable combination of resin type, block copolymer type, interpolymer type, and rubber concentration in the formulation is required to obtain an easy, fast and homogeneous blend. For example, KRATON G-1650, a medium molecular weight polymer with 30 percent polystyrene content, can be easily mixed in a Z-blade mixer with PICCOTAC 95, an aliphatic hydrocarbon resin. A similar polymer described in the examples, polymer A, is a high molecular weight polymer with 33 percent polystyrene content and can easily and quickly be homogeneously blended with REGALITE V-1100. In this case, the aromaticity of the resin helps to dissolve the polymer. However, this blend is not phase stable when aged for several days at elevated temperature. An aliphatic resin, like PICCOTAC 95 or a hydrogenated pure aromatic resin containing low level of aromaticity like REGALREZ 1085 can be used to get homogeneous blends.



Suitable plasticizers include plasticizing oils like low aromatic content (carbon aromatic distribution  $\leq 5\%$ , preferably  $\leq 2\%$ , more preferably  $0\%$  as determined according to DIN 51378) hydrocarbon oils that are

5 paraffinic or naphthenic in character. Those products are commercially available from Shell Oil Company, like SHELLFLEX, CATENEX, ONDINA oils, KAYDOL oil from Witco, or TUFFLO oils from Arco (SHELLFLEX, CATENEX, ONDINA, KAYDOL and TUFFLO are trademarks). Other plasticizers

10 include compatible liquid tackifying resins like REGALREZ R-1018. Other ingredients might also be added, like olefin oligomers, low molecular weight polymers ( $\leq 30,000$  g/mol) like liquid polybutene or liquid polyisoprene copolymers, like liquid styrene/isoprene

15 copolymers or hydrogenated styrene/isoprene copolymers and liquid alpha-olefin polymers, vegetable oils and their derivatives, paraffin and microcrystalline waxes.

It is known in the art that various other components can be added to modify e.g. the odor, and/or the color of

20 the adhesives. Antioxidants and other stabilizing ingredients can also be added to protect the adhesive from degradation induced by heat, light and processing or during storage. Several types of antioxidants can be used, either primary antioxidants like hindered phenols

25 or secondary antioxidants like phosphite derivatives or blends thereof. Examples of commercially available antioxidants are IRGANOX 565 from Ciba-Geigy (2,4-bis-(n-octylthio)-6-(4-hydroxy-3,5-di-tertiary-butyl anilino)-1,3,5-triazine), IRGANOX 1010 from Ciba-Geigy (tetrakis-

30 ethylene-(3,5-di-tertiary-butyl-4-hydroxy-hydrocinnamate)methane) and POLYGUARD HR from Uniroyal (tris-(2,4-di-tertiary-butyl-phenyl)phosphite) (IRGANOX and POLYGUARD are trademarks).

The adhesive composition of the present invention

35 preferably has a viscosity of 100 to 10,000 cPs at

177 °C, more preferably from 600 to 6,000 cPs at 177 °C. The adhesive typically exhibits no transfer after being peeled away from a fabric. The adhesive composition is used in articles such as disposable diapers, sanitary napkins, bed pads, incontinent pads, surgical drapes, plasters, bandages, and the like.

#### EXAMPLES

KRATON G-1650 is a hydrogenated styrene-butadiene-styrene block copolymer having a weight average molecular weight of 109,000, a polystyrene content of 30 percent by weight, and polystyrene block weight average molecular weight of 10,000. Polymer A is a hydrogenated styrene-butadiene-styrene block copolymer having a weight average molecular weight of 286,000, a polystyrene content of 33 percent by weight, and a polystyrene block weight average molecular weight of 29,000. Two different types of metallocene interpolymers were tested, an ethylene-butene-1 copolymer (sold under the trademark EXACT) and several ethylene/octene-1 copolymers (sold under the trademark ENGAGE). The table below shows the properties of these polymers.  $M_n$  is the number average molecular weight,  $M_w$  is the weight average molecular weight,  $M_w/M_n$  is a measure of the polydispersity, and MFI is the melt flow index expressed in dg/min at 190 °C/2.16 kg. Several hydrocarbon tackifying resin types were also evaluated.

Grade	density g/cm <sup>3</sup>	MFI dg/min	$M_n$	$M_w$	$M_w/M_n$
ENGAGE 8100	0.87	1	103,557	179,704	1.735
ENGAGE 8200	0.87	5	65,696	122,262	1.861
ENGAGE 8400	0.87	30	39,930	82,881	2.076
EXACT 4049	0.873	45	57,005	122,743	2.153

Example 1Adhesive properties of KRATON G-1650 and Polymer A with ENGAGE 8400

5 All the ingredients were compounded in a Z-blade mixer. Then the samples were put in beaker in an oven at 180 °C. Once molten, the adhesive was poured onto a Mylar sheet and cast to obtain a thickness of 2 mils (50  $\mu$ m). Prior to testing, the samples were conditioned at 23 °C and 50% RH (relative humidity) for 24 hours.

10 Standard peel, tack and cohesion tests were carried out on these formulations. To assess the right functionality of the adhesive, specific adhesion tests on fabrics were performed, namely to evaluate the adhesion of the positioning adhesive onto the undergarment. Cotton and nylon fabrics are the two reference materials used in  
15 these tests.

The following peel adhesion tests on fabric were carried out:

- 20 - Peel adhesion initial: for cotton, the initial peel is preferred to be in the range of 200-500 g/lineal inch (77-193 N/m).
- Peel adhesion retention or ageing test: the samples (fabric/adhesive/Mylar) are put in an oven at 40 °C for 8 hours under a load of 160 g/sq. in. (24.8 g/cm<sup>2</sup>). Peel  
25 adhesion is determined after 1 hour conditioning at 23 °C and 50% RH. Occurrence of adhesive transfer is also reported as none or transfer.
- Adhesive transfer: the samples (fabric/adhesive/Mylar) are put in oven at 40 °C for 24 hours under a load  
30 of 800 g/sq. in. (124 g/cm<sup>2</sup>). Peel adhesion is determined after 1 hour conditioning at 23 °C and 50% RH. Occurrence of adhesive transfer is also reported as none or transfer.

The SAFT (shear adhesion failure temperature) was measured by 1" x 1" (2.5 x 2.5 cm) Mylar to Mylar lap joint with a 1 kg weight. SAFT measures the temperature at which the lap shear assembly fails under load. Rolling Ball Tack (RBT) is the distance a steel ball rolls on the adhesive film with a standard initial velocity (Pressure Sensitive Tape Council Test No. 6). Small numbers indicate aggressive tack. Holding Power (HP) is the time required to pull a standard area ( $\frac{1}{2}$  in. x  $\frac{1}{2}$  in.) (1.3 x 1.3 cm) of tape from a standard test surface (steel, Kraft paper) under a standard load (1 kg), in shear at 2° (Pressure Sensitive Tape Council Method No. 7). Long times indicate high adhesive strength. 180° peel was determined by Pressure Sensitive Tape Council Method No. 1. Large numbers indicate high strength when peeling a test tape from a steel substrate. Polyken probe tack (PPT) was determined by ASTM D-2979. Loop tack (LT) was determined using PSTC-5 loop tack method. High numbers for PPT and LT indicate aggressive tack. T-peel is measured by ASTM D-1876.

Table 1 below shows the results for KRATON G-1650 and Polymer A (F-1, F-4) and for blends with ENGAGE 8400 in the other columns (F-2, F-3, F-5, F-6). PICCOTAC 95 is a trademark for an aliphatic hydrocarbon tackifying resin which is manufactured by Hercules. V-1100 is a hydrogenated mixed cyclic aromatic tackifying resin which is manufactured by Hercules. TUFFLO 6056 oil is a plasticizing oil which is manufactured by ARCO.

Table 1

Formulation	F-1	F-2	F-3	F-4	F-5	F-6
KRATON G-1650	100	75	50			
Polymer A				100	75	50
ENGAGE-8400		25	50		25	50
PICCOTAC 95	349	349	349			
V-1100				464	464	464
TUFFLO 6056	183	183	183	276	276	276
IRGANOX 1010	3	3	3	3	3	3
Hot Melt Visc. cPs	1,830	1,185	1,025	4200	1243	760
180 Peel (steel) pli (N/m)	4.7 (823)	3.5 (613)	5.1 (893)	2.8 (490)	6.8 (1190)	3.6 (630)
180 Peel Failure	Ghost- ing	Ghost- ing	Cohe- sive	Cohe- sive	Cohe- sive	Cohe- sive
HP Steel, 1 kg (min)	39	14	12	391	72	7
	A/G	PA	Cohe- sive	PC	Cohe- sive	Cohe- sive
SAFT Mylar 0.5 kg	67	52	42	65	57	39
Loop Tack oz/in	42	105	120	101	123	128
N/m	460	1150	1314	1106	1347	1402
Adhesion initial						
T-Peel (cotton) pli	0.5	0.6	0.7	1.2	1.5	2.3 T
T-Peel (cotton) N/m	88	105	123	210	263	403 T
T-Peel (nylon) pli	0.8	0.6	0.9	1.4	1.3	2.5 T
T-Peel (nylon) N/m	140	105	159	245	228	438
Retention						
Aged T-Peel (cotton) pli	0.34	0.5	0.6		2	1.4 T
Aged T-peel (cotton) N/m	60	88	105		350	245

Table 1 (Cont'd)

Formulation	F-1	F-2	F-3	F-4	F-5	F-6
Aged T-Peel (nylon) pli	0.7	0.7	1		1.2	1.7 T
Aged T-peel (nylon) N/m	123	123	175		210	298
Transfer						
T-Peel (cotton) pli	0.81		1.04	1.42		
T-peel (cotton) N/m	142		184	249		
T-Peel (nylon) pli	1.05		1.34	1.28		
T-peel (nylon) N/m	184		235	224		

T = transfer; A/G = adhesive/ghosting; PA = partial adhesive; PC = partial cohesive

#### KRATON G-1650/ENGAGE 8400

Comparison of F-1, 2 and 3 indicates that the use of up to 50% of the metallocene interpolymer does not change the adhesion properties on fabric. Indeed, adhesion initial, retention, and transfer are almost equivalent. Hot melt viscosity, holding power, and SAFT are lower than without the interpolymer. The decrease in hot melt viscosity is very attractive because of the trend to go for lower application temperature systems. The decrease in holding power and SAFT is not considered desirable, although no transfer was observed in our testing conditions.

#### Polymer A/ENGAGE 8400

Comparison of F-4, 5 and 6 indicates that at 50/50 ratio Polymer A/ENGAGE 8400, there is adhesive transfer on fabric, even without aging but not at a ratio 75/25. Other properties, like hot melt viscosity, holding power, and SAFT are lower than without the interpolymer. Thus, smaller amounts of the interpolymer can be used with Polymer A but not as much as with KRATON G-1650.

Transfer test

For all the transfer tests on fabric, the peel  
adhesion profile on cotton is always smoother than that  
on nylon. This is particularly obvious when the peel  
5 adhesion is below about 1 pli (175 N/m) and when no  
transfer or very slight transfer is observed.

For medium transfer, the peel adhesion is much higher  
and no difference can be observed between the two  
fabrics. Indeed, the adhesive has flowed intensively  
10 through the meshes of the fabric and makes strong bonds  
with the fabric. The cohesive failure of the adhesive is  
the main phenomenon that is recorded.

Example 2

Adhesive properties of Polymer A and Engage 8400 with  
15 different tackyfying resin

This series of test shows that the type of resin used  
in the formulation influences greatly the end properties.  
Indeed, F-8, compounded with a R-6108, hydrogenated pure  
aromatic resin, gives much better properties than F-7,  
20 compounded with a mixed cyclic/aromatic resin, V-1100.  
There is no transfer and the adhesion on fabric is  
excellent. Compared to F-3, SAFT and holding power are  
equivalent. After about 4 days storage at 177 °C,  
Formulation F-8 (Polymer A/Engage 8400) shows phase  
25 separation. However, the same formulation, compounded  
either with an aliphatic hydrocarbon resin, like  
PICCOTAC 95, or an hydrogenated aromatic resin, like  
REGALREZ 1085, does not show phase separation when  
submitted to the same test. This indicates that a careful  
30 selection of the appropriate resins, with the right  
balance in aliphatic/aromatic character, is needed to  
achieve the best compatibility between all the  
ingredients.

Table 2

Formulation	F-7	F-8
Polymer A	50	50
E-8400	50	50
R-6108		464
V-1100	464	
TUFFLO 6056	276	276
IRGANOX 1010	3	3
Hot Melt Visc. cPs	760	1,593
180 Peel (steel) pli (N/m)	3.6 (630)	3.6 (630)
Formulation	F-7	F-8
180 Peel Failure	Cohesive	Cohesive
HP Steel, 1 kg (min)	7	13
HP failure	Cohesive	Cohesive
SAFT Mylar 0.5kg	39	40
Loop Tack oz/in (N/m)	128 (1402)	136 (1489)
Adhesion initial		
T-Peel (cotton) pli	2.3 T	0.9
T-Peel (cotton) N/m	403 T	159
T-Peel (nylon )pli	2.5 T	0.9
T-Peel (nylon) N/m	438	159
Retention		
Aged T-Peel (cotton) pli	1.4 T	0.9
Aged T-peel (cotton) N/m	245	159
Aged T-Peel (nylon) pli	1.7 T	0.9
Aged T-peel (nylon) N/m	298	159
Transfer		
T-Peel (cotton) pli		0.8
T-peel (cotton) N/m		140
T-Peel (nylon) pli		0.9
T-peel (nylon) N/m		159

T = transfer



Example 3Adhesive properties of KRATON G-1650 with ENGAGE 8400, ENGAGE 8200, ENGAGE 8100 blends

5 This series of test has been done to assess the influence of the melt flow index and the molecular weight of the ENGAGE grades on the adhesive properties of positioning adhesives. By replacing part by part ENGAGE 8400 by other ENGAGE grades which have a lower melt flow index, it can be seen that again, the adhesion properties are not affected, but the hot melt viscosity, the SAFT and the holding power increased as expected because the molecular weight of the ENGAGE grades is also increased.

Table 3

Formulation	F-9	F-19	F-11
KRATON G-1650	50	50	50
E-8400	50		
E-8200		50	
E-8100			50
PICCOTAC 95	349	349	349
TUFFLO 6056	183	183	183
IRGANOX 1010	3	3	3
Hot Melt Visc. cPs	1,025	2,160	4,190
180 Peel (steel)	5.1	6.4	5.5
180 Peel Failure	Cohesive	Cohesive	Ghosting
HP Steel, 1 kg (min)	12	14	22
HP Failure	Cohesive	Cohesive	Cohesive
SAFT Mylar 0.5 kg	42	41	48
Loop Tack oz/in (N/m)	120 (1314)	110 (1205)	111 (1215)

Table 3 (Cont'd)

Formulation	F-9	F-19	F-11
Adhesion initial			
T-Peel (cotton) pli	0.7	0.6	0.6
T-peel (cotton) N/m	123	105	105
T-Peel (nylon) pli	0.9	0.8	0.8
T-peel (nylon) N/m	159	140	140
Retention			
Aged T-Peel (cotton) pli	0.6	0.8	0.6
Aged T-peel (cotton) N/m	105	140	105
Aged T-Peel (nylon) pli	1	0.8	0.8
Aged T-peel (nylon) N/m	175	140	140
Transfer			
T-Peel (cotton) pli	1.04		
T-peel (cotton) N/m	182		
T-Peel (nylon) pli	1.04		
T-peel (nylon) N/m	182		

Example 4Adhesive properties of KRATON G-1650 and EXACT 4049

5 This series compare the adhesive properties obtained with the addition of ethylene/butene-1 copolymer, EXACT 4049. All the adhesive properties look good, particularly the absence of any transfer on fabric.

Table 4

Formulation	F-12	F-13
KRATON G-1650	100	50
EXACT-4049		50
PICCOTAC 95	349	349
TUFFLO 6056	183	183
IRGANOX 1010	3	3

Table 4 (Cont'd)

Formulation	F-12	F-13
Hot Melt Visc. CPs	1,830	3,245
180 Peel (steel) pli (N/m)	4.7 (823)	5 (875)
180 Peel Failure	Ghosting	Ghosting
HP Steel, 1 kg (min)	39	27
	A/G	Cohesive
SAFT Mylar 0.5 kg	67	40
Loop Tack oz/in (N/m)	42 (460)	135 (1478)
Adhesion initial		
T-Peel (cotton) pli	0.5	0.6
T-Peel (cotton) N/m	88	105
T-Peel (nylon) pli	0.8	0.8
T-Peel (nylon) N/m	140	140
Retention		
Aged T-Peel (cotton) pli	0.34	0.7
Aged T-peel (cotton) N/m	60	123
Aged T-Peel (nylon) pli	0.7	1
Aged T-peel (nylon) N/m	123	175
Transfer		
T-Peel (cotton) pli	0.81	1
T-peel (cotton) N/m	142	175
T-Peel (nylon) pli	1.05	1.1
T-peel (nylon) N/m	184	193

Example 5-Comparative Example

The same tests were carried out with four other block copolymers. The first is KRATON G-1652 polymer which has a weight average molecular weight of 79,000, polystyrene block weight average molecular weight of 7100, and polystyrene content of 30 percent by weight. Polymer B is a radial polymer having two hydrogenated styrene-

butadiene arms and two unhydrogenated isoprene arms. The weight average molecular weight is 187,000, the polystyrene block weight average molecular weight is 11,500, and the polystyrene content 18 percent. KRATON G-1726 polymer is an SEBS polymer having a weight average molecular weight of 73,000, a polystyrene block weight average molecular weight of 7100, a polystyrene content of 31 percent, and which has a coupling efficiency of 30 percent (this means that only 30 percent of the total polymer is triblock and the rest is diblock). The fourth polymer is SEPTON 4033 polymer made by Kuraray (hydrogenated styrene-isoprene-styrene, SEPS) which has a weight average molecular weight of 96,000, a polystyrene block weight average molecular weight of 8100, and a polystyrene content of 28 percent by weight. KRATON G-1652 was not acceptable at a 50:50 weight ratio but the formulation at 85:15 KRATON G-1652:EXACT-8400 worked well. It can be seen that neither 1726 nor Polymer B used alone are acceptable because they produce adhesives which transfer to the fabric. However, the blend of KRATON G-1652 and KRATON G-1726 worked well. SEPTON 4033 is acceptable because the properties are good and there is no transfer (SEPTON is a trademark).

Table 5

[illegible]

Table 5 (Cont'd)

Formulation	F-1	F-14	F-15	F-16	F-17	F-18	F-19	F-20
TUFFLO 6056	183	183	183	183	183	183	183	183
IRGANOX 1010	3	3	3	3	3	3	3	3
Hot Melt Visc cPs	1,025	620	1,450	159	644	898	590	638
180° Peel (steel) pli (N/m)	5.1 (893)	4.9 (858)	7.8 (1365)	3 (525)	4.1 (718)	4.7 (823)	--	--
180° Peel Failure	cohe- sive	cohe- sive	cohe- sive	cohe- sive	cohe- sive	cohe- sive	--	--
HP Steel, 1 kg (min)	12	12	61	0.8	1	6	--	--
HP Failure	cohe- sive	cohe- sive	cohe- sive	cohe- sive	cohe- sive	cohe- sive	--	--
SAFT Mylar 0.5 kg	42	40	40	40	39	39	--	--
Loop Tack oz/in	120	142	155	96	192	119	--	--
N/m	1314	1555	1697	1051	2102	1303		
Adhesion initial								
T-Peel (cotton) pli	0.7	0.5	0.8	1.3 ST	1.5 T	0.5	0.6	0.8
T-Peel (cotton) N/m	123	88	140	228	263	88	105	140
T-Peel (nylon) pli	0.9	0.7	0.9	1.2 ST	1.5 T	1	0.3	0.5
T-Peel (nylon) N/m	154	123	154	210 ST	263 T	175	53	88

Table 5 (Cont'd)

Formulation	F-1	F-14	F-15	F-16	F-17	F-18	F-19	F-20
Retention								
Aged T-Peel (cotton) pli	0.6	2.2 T	4 T		1.6 T	1.3	0.7	0.8
Aged T-Peel (cotton) N/m	105	385 T	700		280 T	228	123	140
Aged T-Peel (nylon) pli	1	2.9 T	2.2 T		1.7 T	1.5	0.7	0.9
Aged T-Peel (nylon) N/m	175	508 T	385		298	263	123	154
Transfer								
24 hr. T-Peel (cotton) pli	1.04					1.3	1.2	0.9
24 hr. T-Peel (cotton) N/m	182					228	210	154
24 hr. T-Peel (nylon) pli	1.34					1.5	1.2	1
24 hr. T-Peel (nylon) N/m	235					263	210	175

Example 6

In this example, blends of various tackifying resins with varying MMAPcloud point values were tested with several block copolymers and interpolymers for phase stability. The results are shown in Table 6 below.

Table 6

Compatibility SBC/resin/metallocene blends in function of the aromaticity of the resin as defined by the MMAP cloud point

	R-3102	V-1100 E-8400	R-6108 E-8400	R-1085 E-4049	PICCOTAC 95 E-4049
MMAP °C	24	48	54	85	95
KRATON G-1650	I	C	-	C	C
Polymer A	I	I	I	C	C

I = INCOMPATIBLE

C = COMPATIBLE

Example 7

In this experiment, two blends of the block copolymer and interpolymers were compared with the neat block copolymer in respect of their viscosity/temperature profiles. It can be seen from the results shown in Table 7 below that both of the blends are lower in viscosity at lower temperatures. This is precisely the desired advantage so that the adhesives containing them can be more easily processed at lower temperatures.

Table 7

Temperature °F (°C)	G-1650-15.7%	G-1650/E-8400	G-1650/E-4049
275 (135)	73,300	11,075	37,800
300 (149)	16,240	4,600	14,480
325 (163)	4,570	1,985	6,760
350 (177)	1,800	1,039	3,245

Example 8

The same tests were carried out with four other polymers. Polymer C is a styrenic block copolymer which has a molecular weight of 79,000, a polystyrene block molecular weight of 7100, a polystyrene content of 30

percent by weight and a butylene content of about 70%.

RP-6924 is a styrenic block copolymer which has a molecular weight of 140,000, a polystyrene block molecular weight of 10,000, a polystyrene content of 20 percent by weight and a butylene content of about 70%.

Polymer D is a styrenic block copolymer which has a molecular weight of 148,000, a polystyrene block molecular weight of 7,400, a polystyrene content of 16 percent by weight, and a butylene content of about 70%. KRATON G-1657 is a styrenic block copolymer which has a molecular weight of 148,000, a polystyrene block molecular weight of 5,300, a polystyrene content of 13 percent by weight, and a diblock content of 35 percent by weight. Polymer C (Formulation F-21) and Polymer D (Formulation F-24) show good peel adhesion properties on cotton and nylon without adhesive transfer onto these fabrics for a ratio polymer/polyolefin 85/15% by weight. At another ratio, namely 50/50% by weight, Formulation F-22, the formulation shows adhesive transfer. However, RP-6924 at a ratio of 50/50% by weight shows good peel adhesion on cotton and nylon without adhesive transfer onto these fabrics. KRATON G-1657 based formulations (Formulations F-25 and F-26) show adhesive transfer on cotton and nylon and fail for this test.

Table 8

Ingredients	F-21	F-22	F-23	F-24	F-25	F-26
Polymer C	15	50				
KRATON G-6924			50			
Polymer D				15		
KRATON G-1657					15	50
ENGAGE 8200	85	50	50	85	85	50
PICCOTAC 95	349					
ONDINA 68	183					



Table 8 (Cont'd)

Ingredients	F-21	F-22	F-23	F-24	F-25	F-26
IRGANOX 1010	3					
Properties						
<u>Adhesion Initial</u>						
T-Peel cotton N/m	45	95	60	60	85	100
T-Peel nylon N/m	155	195	120	125	155	175T
<u>Retention</u>						
T-Peel cotton N/m	170	560T	140	180	190	500T
T-Peel nylon N/m	290	400	240	320	310	520T
<u>Transfer</u>						
T-Peel cotton N/m	275	640T	390	330	560T	560T
T-Peel nylon N/m	360	640T	350	380	390	560T

T = Adhesive transfer onto fabric

#### Example 9

In this experiment, blends of block copolymer with elevated butylene and interpolymer Engage 8200 were compared with the neat block copolymer in respect of their viscosity/temperature profile. It can be seen in Table 9 that the reported viscosities are low. It should also be recognized that the formulation F-19 that contains a blend KRATON G-1650/Engage 8200 has a hot-melt viscosity of 2160 at 177 °C, higher than those reported in Table 9 for the same temperature.

Table 9

Temperature	Engage 8200/ P-5828	Engage 8200/ P-6924	Engage 8200/ P-7297
	cPs	cPs	cPs
120°C	14,000	26,300	13,300
140°C	5,600	6,360	5,540
160°C	2,820	1,800	2,690
177°C	1,700	960	1,620

C L A I M S

1. A hot melt pressure sensitive positioning adhesive for use with an absorbent article which comprises:
- (a) from 5 to less than 15 percent by weight basis the total of (a), (b) and (c), of a blend of
- 5 (i) a selectively hydrogenated styrene-(butadiene and/or isoprene)-styrene block copolymer having either (I) a polystyrene block number average molecular weight of 20,000 or less, or (II) having a polystyrene block number average molecular weight greater than 20,000 and
- 10 (ii) a homogeneous linear or substantially linear interpolpolymer of ethylene and at least one C<sub>3</sub>-C<sub>20</sub> alpha olefin having a density from 0.85 to 0.91 grams per cubic centimeter; and
- (b) from 50 to 80 percent by weight, basis the total of
- 15 (a), (b) and (c), of a tackifying resin which has an aromaticity such that the MMAP cloud point is either (I) at least 45 °C or (II) at least 70 °C; and
- (c) from 5 to 35 percent by weight basis the total of (a), (b) and (c), of a plasticizer.
- 20 2. The adhesive of claim 1 wherein the blend of (a) contains a block copolymer (i) having a polystyrene block number average molecular weight in the range of more than 9,500 to 20,000 and a total number average molecular weight of more than 95,000 to 300,000.
- 25 3. The adhesive of claim 1 or 2 wherein the blend of (a) contains the block copolymer (i) and interpolpolymer (ii) in a weight ratio of from 90:10 to 10:90.
4. The adhesive of claim 3 wherein the blend of (a) contains block copolymer and interpolpolymer in a weight
- 30 ratio of from 80:20 to 20:80.

5. The adhesive of claim 1 or 2 wherein the block copolymer of (i) also contains from 5 to 40 percent by weight of a second block copolymer which has a diblock content of at least 70 percent by weight.

5 6. The adhesive composition of claim 1 or 2 wherein the block copolymer of (i) has a polystyrene content of more than 25 percent by weight and has added to it from 5 to 40 percent by weight of a second block copolymer having a polystyrene content of less than 25 percent by weight.

10 7. The adhesive of claim 6 wherein the polystyrene content of the second block copolymer is 22 percent by weight or less.

8. The hot melt adhesive of claim 1 or 2 wherein the viscosity of the adhesive is from 100 to 10,000 cPs at 177 °C and the adhesive exhibits no transfer after being  
15 peeled away from a fabric.

9. The adhesive of claim 1 wherein the blend of (a) contains a block copolymer having a polystyrene block number average molecular weight of 5500 to 9500 and a  
20 total molecular weight of 65,000 to 95,000 and interpolymer in a weight ratio of from 60:40 to 90:10.

10. The adhesive of claim 9 wherein the blend of (a) contains said block copolymer and interpolymer in a weight ratio of from 80:20 to 90:10.

25 11. Absorbent article comprising a hot melt pressure sensitive positioning adhesive as claimed in any one of claims 1-10.

# INTERNATIONAL SEARCH REPORT

International Application No

PCT/EP 00/05902

**A. CLASSIFICATION OF SUBJECT MATTER**  
IPC 7 A61L15/58

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 A61L C08L C09J

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, PAJ, FSTA, INSPEC, COMPENDEX, CHEM ABS Data, EMBASE, MEDLINE

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 5 171 793 A (MAROIE SERGE ET AL) 15 December 1992 (1992-12-15) column 6, line 4 - line 63 ---	1-11
Y	EP 0 716 124 A (SHELL INT RESEARCH) 12 June 1996 (1996-06-12) page 3, line 7 - line 42 example 1 ---	1-11
Y	US 5 331 038 A (DILLMAN STEVEN H) 19 July 1994 (1994-07-19) abstract column 3, line 44 - column 4, line 40 ---	1-4, 8-10
Y	EP 0 822 227 A (SHELL INT RESEARCH) 4 February 1998 (1998-02-04) page 2, line 51 - page 3, line 10 page 4, line 20 - line 48 ---	1-4, 8-10
	-/--	

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

\* Special categories of cited documents:

\*A\* document defining the general state of the art which is not considered to be of particular relevance

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\*O\* document referring to an oral disclosure, use, exhibition or other means

\*P\* document published prior to the international filing date but later than the priority date claimed

\*T\* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

\*X\* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

\*Y\* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

\*&\* document member of the same patent family

Date of the actual completion of the international search

10 November 2000

Date of mailing of the international search report

24/11/2000

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2  
NL - 2280 HV Rijswijk  
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl.  
Fax: (+31-70) 340-3016

Authorized officer

Menidjel, R

# INTERNATIONAL SEARCH REPORT

International Application No

PCT/EP 00/05902

## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p>US 4 904 728 A (GEORGE ERIC R)  27 February 1990 (1990-02-27)  column 5, line 58 -column 6, line 56  column 8, line 18 - line 52  -----</p>	1-11

## FURTHER INFORMATION CONTINUED FROM PCT/ISA/ 210

## Continuation of Box I.2

Present claims 1,8 relate to a product/compound defined by reference to a desirable characteristic or property, namely the resin has an aromaticity such that the MMAP cloud point is at least 45°C, the viscosity of the adhesive is from 100 to 10,000 cPs at 177°C and exhibits no transfer after being peeled away from a fabric.

The claims cover all products/compounds having these characteristics or properties, whereas the application provides support within the meaning of Article 6 PCT and/or disclosure within the meaning of Article 5 PCT for only a very limited number of such products/compounds. In the present case, the claims so lack support, and the application so lacks disclosure, that a meaningful search over the whole of the claimed scope is impossible. Independent of the above reasoning, the claims also lack clarity (Article 6 PCT). An attempt is made to define the product/compound by reference to a result to be achieved. Again, this lack of clarity in the present case is such as to render a meaningful search over the whole of the claimed scope impossible. Consequently, the search has been carried out for those parts of the claims which appear to be clear, supported and disclosed, namely those parts relating to the products/compounds prepared in examples 1-9.

The applicant's attention is drawn to the fact that claims, or parts of claims, relating to inventions in respect of which no international search report has been established need not be the subject of an international preliminary examination (Rule 66.1(e) PCT). The applicant is advised that the EPO policy when acting as an International Preliminary Examining Authority is normally not to carry out a preliminary examination on matter which has not been searched. This is the case irrespective of whether or not the claims are amended following receipt of the search report or during any Chapter II procedure.

# INTERNATIONAL SEARCH REPORT

International Application No

PCT/EP 00/05902

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